

## Differential Equations of Motion of the Particle

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### Abstract

*This paper deals with linearised and normalized differential equations of relative motion of the system under the influence of magnetic force air resistance and oblateness of the earth in Nechvill's co-ordinate system. We have linearised the problem keeping in view that the length of the string connecting the two satellites is infinitesimally small in comparison to the distance of centre of mass of the system from the centre of attracting force and introduction of rotating frame of reference eliminates the product terms as usual. We have obtained a system of six orders non-autonomous, non-linear equations of motion describe the motion of one of two satellites and the motion of satellite relative to the first may easily be obtained by  $m_1 \vec{\rho}_1 + m_2 \vec{\rho}_2 = 0$*

**Keywords:** differential equations of motion, frame of reference, linearized, normalized, oblateness

### Introduction

A light, flexible, and extensible wire is placed in the center of the earth's gravitational field to connect the effects of air resistance, magnetic force, and the earth's oblateness on the motion of the satellites. The system's motion is investigated in relation to its center of mass, which is thought to be travelling along a Keplerian orbit. The differential equations of motion of the system under the effect of air resistance, magnetic force, and earth's oblateness have been determined using the first kind of Lagrange's equations of motion. The normalized and linearized differential equations for the mass of the system's particle  $m_1$  were developed under the

presumption that the connecting cable's length is very little in comparison to the satellites' distance from the planet's center Fletcher (1965). Then differential equations of motion in rotating frame of reference obtained. After using Nechvill's co-ordinate system, a set of non-autonomous, non-homogeneous differential equations of the particle of mass  $m_1$  of the system derived (Elsogotts, 1973).

### Equations of Motion of the centre of mass

Let's think about how a system of particles with masses  $m_1$  and  $m_2$ , respectively, would move in the earth's gravitational field if they were connected by a thin, flexible, and extensible string. Let  $\vec{r}_1$  and  $\vec{r}_2$  be their radius vectors with respect to the centre of the earth (Etkin, 1964).

Then, using the first type of Lagrange's equations for motion, we formulate the differential equations for the motion of the particles with masses  $m_1$  and  $m_2$  as.

$$m_1 \ddot{r}_1 + \frac{m_1 \mu \vec{r}_1}{r_1^3} + \lambda \left[ \frac{|\vec{r}_1 - \vec{r}_2| - l_0}{l_0} \right] \frac{(\vec{r}_1 - \vec{r}_2)}{|\vec{r}_1 - \vec{r}_2|} = 0$$

$$\text{and } m_2 \ddot{r}_2 + \frac{m_2 \mu \vec{r}_2}{r_2^3} - \lambda \left[ \frac{|\vec{r}_1 - \vec{r}_2| - l_0}{l_0} \right] \frac{(\vec{r}_1 - \vec{r}_2)}{|\vec{r}_1 - \vec{r}_2|} = 0 \quad (1)$$

Where  $\lambda$  is the Hook's modulus of elasticity and  $\mu$  is the product of gravitational constant with the mass of attracting center.

The condition of constraint is given by

$$|\vec{r}_1 - \vec{r}_2|^2 \leq l_0^2 \quad (2)$$

where  $l_0$  is the string's natural length between the two satellites with masses  $m_1$  and  $m_2$

If the equality signs in (2) holds; then  $\lambda \neq 0$  and the motion takes place with tight string and consequently tension in the string comes into play.

### Motion of the System Relative to their Centre of Mass

In order to study the relative motion of the system, we must predict about the motion of the centre of mass in the beginning itself (Chernouske, 1963, 1964).

Let  $\vec{R}$  be the radius vector of the centre of mass of the system w.r.to the attracting center (Earth). Then we have

$$\vec{R} = \frac{m_1 \vec{r}_1 + m_2 \vec{r}_2}{m_1 + m_2} \quad (3)$$

Adding the two equations of (1) we get

$$M \ddot{\vec{R}} + \mu \left( \frac{m_1 \vec{r}_1}{r_1^3} + \frac{m_2 \vec{r}_2}{r_2^3} \right) = 0 \quad (4)$$

Where  $M = m_1 + m_2$

Now we shall make use of the assumption that the maximum extended length  $l_E$  of the string is infinitesimally small compared to the distances  $r_1$  and  $r_2$  of the particles from the centre of force.

$$\text{i.e.} \quad \frac{l_E}{r_1} \ll 1 \text{ and } \frac{l_E}{r_2} \ll 1 \quad (5)$$

Let  $\vec{\rho}_1$  and  $\vec{\rho}_2$  denote the radius vector of the particles of mass  $m_1$  and  $m_2$  respectively with origin at the centre of mass of the system (Sharma, 1974).

$$\begin{aligned} \text{Then,} \quad \vec{r}_1 &= \vec{R} + \vec{\rho}_1 \\ \vec{r}_2 &= \vec{R} + \vec{\rho}_2 \end{aligned} \quad (6)$$

Then clearly  $\rho_1 < l_E$

$$\rho_2 < l_E$$

Thus  $\rho_1 \ll r_1$

and  $\rho_2 \ll r_2$

But  $r_1 \approx r_2 \approx R$

Hence  $\frac{\rho_1}{R} \ll 1$  and  $\frac{\rho_2}{R} \ll 1$  (7)

Eliminating  $\vec{r}_1$  and  $\vec{r}_2$  from (4) with the help of (6) and then expanding in ascending particles of small equalities.

$\frac{\rho_1}{R}$  and  $\frac{\rho_2}{R}$  we get

$$M \ddot{\vec{R}} + \frac{\mu M \vec{R}}{R^3} = \vec{F}_1 + \vec{F}_2 + 0(3) \quad (8)$$

Where  $\vec{F}_1 = \frac{3\mu}{R^3} (m_1 \vec{\rho}_1 + m_2 \vec{\rho}_2) - \frac{3\mu}{R^5} [\vec{R} (m_1 \vec{\rho}_1 + m_2 \vec{\rho}_2)] \vec{R}$

$$\vec{F}_2 = -\frac{3}{2} \frac{\mu}{R^3} \left[ m_1 \left\{ \left( \frac{\rho_1}{R} \right)^2 - 5 \left( \frac{\vec{R} \vec{\rho}_1}{R R} \right) \right\} + m_2 \left\{ \left( \frac{\rho_2}{R} \right)^2 - 5 \left( \frac{\vec{R} \vec{\rho}_2}{R R} \right)^2 \right\} \right] \vec{R} \quad (9)$$

(3) stands for third and higher order terms in infinitesimals  $\frac{\rho_1}{R}$  and  $\frac{\rho_2}{R}$

## Equations of Motion of the System under the Influence of AIR Resistance Magnet

### Force. In the Central Gravitational of Oblate Earth

Let's imagine that the two satellites of the system are particles with masses of  $m_1$  and  $m_2$  and their radius vectors  $\vec{r}_1$  and  $\vec{r}_2$  respectively, in relation to the attractive center (Beletaky & Novicova, 1969). The length of the string connecting the two particles of mass  $m_1$  and  $m_2$  be denoted by  $l_0$ . Suppose that 'l' be the string length at any time (Karn, 2002).

Then the constraint of system is given by

$$\left| \vec{r}_1 - \vec{r}_2 \right|^2 \leq l_0^2 \quad (10)$$

Under the inspiration of air resistance, magnetic force, and earth's oblateness, the equation of motion of two particles of mass  $m_1$  and  $m_2$  associated by an extendable string of natural length  $l_0$  can be stated using Lagrange's equation of motion of first kind as follows:

$$m_1 \ddot{\vec{r}}_1 + \frac{m_1 \mu \vec{r}_1}{r_1^3} + \frac{3m_1 \mu k_2 \vec{r}_1}{r_1^5} + \lambda \left[ \frac{|\vec{r}_1 - \vec{r}_2| - l_0}{l_0} \right]$$

$$\frac{(\vec{r}_1 - \vec{r}_2)}{|\vec{r}_1 - \vec{r}_2|} = \vec{F}_{a_1} + Q_1(\vec{r}_1 \times \vec{H})$$

$$\text{and } m_2 \ddot{\vec{r}}_2 + \frac{m_2 \mu \vec{r}_2}{r_2^3} + \frac{3m_2 \mu k_2 \vec{r}_2}{r_2^5} - \lambda \left[ \frac{|\vec{r}_1 - \vec{r}_2| - l_0}{l_0} \right] \frac{(\vec{r}_1 - \vec{r}_2)}{|\vec{r}_1 - \vec{r}_2|} = \vec{F}_{a_2} + Q_2(\vec{r}_2 \times \vec{H})$$

Where  $\vec{F}_{ai}$  ( $i = 1, 2, \dots$ ) is the aerodynamic force

$$k_2 = \bar{\epsilon} R_e^2 / 3$$

$$\alpha R = \frac{R_e - R_p}{R_e} = \text{Earth's of oblateness}$$

We have

$$\text{and } \left. \begin{aligned} \vec{\rho}_1 &= \frac{m_2}{m_1 + m_2} (\vec{r}_1 - \vec{r}_2) \\ \vec{\rho}_2 &= \frac{m_1}{m_1 + m_2} (\vec{r}_2 - \vec{r}_1) \end{aligned} \right\} \quad (11)$$

multiplying first equation of (11) say  $m_1$  and equation by  $m_2$  and adding we get.

$$m_1 \vec{\rho}_1 + m_2 \vec{\rho}_2 = 0 \quad (12)$$

Hence  $\vec{F}_1$  given in (9) vanishes identically on using (12). Therefore, neglecting the 2<sup>nd</sup> and higher order agitation relations in (9), the centre of

mass of the system's equation given by (8) takes the system (Chetayev, 1966).

$$\ddot{M}\vec{r} + \frac{\mu M \vec{R}}{R^3} = 0 \quad (13)$$

Clearly (13) demonstrate that the system's center of mass can be anticipated to move with more precision up to and including order-infinitesimal along a Keplerian elliptical orbit (Dubeshin, 1952) i.e.  $\frac{\rho_1}{R}$  and  $\frac{\rho_2}{R}$ .

The center of mass of the system of two satellites connected by an extendable string in the center of the gravitational field of attraction has thus been demonstrated to travel along a specific Keplerian elliptical orbit (Singh, 1971, 1973).  $\bar{\epsilon} = \alpha_R - \frac{m}{2}$  where  $m = \frac{\Omega^2 R_e}{g_e}$

$\Omega$  = Rotational angular velocity of the earth.

$R_e$  = Earth's equatorial radius.

$R_p$  = Earth's polar radius.

$g_e$  = Earth's gravitational field as a function.

$$Q_i = \frac{\text{charge } q_i \text{ on the } i^{\text{th}} \text{ particle}}{\text{Velocity of light } C}; \quad (i = 1, 2)$$

$\vec{F}$  = The earth's magnetic field intensity for equatorial satellites

$$= \frac{-\vec{\nabla}(\vec{m} \cdot \vec{r})}{r^3}$$

$\vec{m}$  = Earth's magnetic moment.

Since it is expected that air drag in this situation varies as the square of the speed of the moving particles (Solue, 1960), it can be expressed as follows:

$$\vec{F}_{a_i} = -\rho_a C_i |\dot{\vec{r}}_0| \dot{\vec{r}}_i \quad (14)$$

Where  $\rho_a$  is the density of the air, which will be assumed constant throughout the study.

$$C_i = \text{Ballistic Coeff}^{\text{th}}$$

Now the equations of motion (2) can be written in the form

$$m_1 \ddot{\vec{r}}_1 + \frac{m_1 \mu \vec{r}_1}{r_1^3} + \frac{3\mu m_1 k_2 \vec{r}_1}{r_1^5} + \lambda \left[ \frac{|\vec{r}_1 - \vec{r}_2| - l_0}{l_0} \right]$$

$$\frac{(\vec{r}_1 - \vec{r}_2)}{|\vec{r}_1 - \vec{r}_2|} = -\rho_a C_1 |\dot{\vec{r}}_1| \dot{\vec{r}}_1 + Q_1 (\dot{\vec{r}}_1 \times \vec{H})$$

and

$$m_2 \ddot{\vec{r}}_2 + \frac{m_2 \mu \vec{r}_2}{r_2^3} + \frac{3m_2 \mu k_2 \vec{r}_2}{r_2^5} - \lambda \left[ \frac{|\vec{r}_1 - \vec{r}_2| - l_0}{l_0} \right] \frac{(\vec{r}_1 - \vec{r}_2)}{|\vec{r}_1 - \vec{r}_2|} = -\rho_a C_2 |\dot{\vec{r}}_2| \dot{\vec{r}}_2 + Q_2 (\vec{r}_2 \times \vec{H}) \quad (15)$$

Linearised and Normalized Differential Equations of Relative motion of the system. We divide the two equations of (4) by  $m_1$  and  $m_2$  respectively and then on subtraction; we get

$$\ddot{\vec{r}}_1 - \ddot{\vec{r}}_2 + \mu \left( \frac{\vec{r}_1}{r_1^3} - \frac{\vec{r}_2}{r_2^3} \right) + \lambda \frac{(m_1 + m_2)}{m_1 m_2} \left[ \frac{|\vec{r}_1 - \vec{r}_2| - l_0}{l_0} \right]$$

$$\frac{(\vec{r}_1 - \vec{r}_2)}{|\vec{r}_1 - \vec{r}_2|} + 3\mu k_2 \left( \frac{\vec{r}_1}{r_1^5} - \frac{\vec{r}_2}{r_2^5} \right) + \rho_a \left[ C_1 |\dot{\vec{r}}_1| \dot{\vec{r}}_1 - C_2 |\dot{\vec{r}}_2| \dot{\vec{r}}_2 \right] = \frac{Q_1}{m_1} (\dot{\vec{r}}_1 \times \vec{H}) - \frac{Q_2}{m_2} (\dot{\vec{r}}_2 \times \vec{H}) \quad (16)$$

using (6) and ignoring minuscules of 2nd and higher order we get

$$u\left(\frac{\vec{r}_1}{r_1^3} - \frac{\vec{r}_2}{r_2^3}\right) = \frac{\mu}{R^3}(\vec{r}_1 - \vec{r}_2) - \frac{3\mu\vec{R}}{R^5}[\vec{R}(\vec{r}_1 - \vec{r}_2)] \quad (17)$$

$$3\mu k_2\left(\frac{\vec{r}_1}{r_1^5} - \frac{\vec{r}_2}{r_2^5}\right) = \frac{3\mu k_2}{R^5}(\vec{r}_1 - \vec{r}_2) - \frac{15\mu k_2}{R^7}[\vec{R}(\vec{r}_1 - \vec{r}_2)]\vec{R} \quad (18)$$

$$\text{and } \rho_a [C_1 |\dot{\vec{r}}_1| \dot{\vec{r}}_1 - C_2 |\dot{\vec{r}}_2| \dot{\vec{r}}_2] = \rho_a \dot{R} \dot{R} (C_1 - C_2) + \rho_a R$$

$$\left[ \frac{\dot{R}(\dot{R} \cdot \vec{\rho}_1 + \dot{\rho})}{R^2} \right] \frac{(C_1 m_2 + C_2 m_1)}{m_2} \quad (19)$$

with the help of (17), (18) and (15) in (16) we get on using

$$\begin{aligned} \vec{H} &= -\frac{\vec{\nabla} \vec{M} \cdot \vec{r}_1}{r_1^3} \text{ for } (i = 1, 2) \\ \ddot{r}_1 - \ddot{r}_2 + \frac{\mu}{R^3}(\dot{r}_1 - \dot{r}_2) - \frac{3\mu\vec{R}}{R^5}[\vec{R}(\dot{r}_1 - \dot{r}_2)] \\ &+ \lambda \left( \frac{m_1 + m_2}{m_1 \times m_2} \right) \left[ \frac{|\vec{r}_1 - \vec{r}_2| - l_0}{l_0} \right] \frac{(\vec{r}_1 - \vec{r}_2)}{|\vec{r}_1 - \vec{r}_2|} \\ &+ \frac{3\mu k_2}{R^5}(\vec{r}_1 - \vec{r}_2) - \frac{15\mu k_2}{R^7} \{ \vec{R}(\vec{r}_1 - \vec{r}_2) \} \vec{R} \\ &+ \rho_a \dot{R} \dot{R} (C_1 - C_2) + \rho_a R \left[ \frac{\dot{R}(\dot{R} \cdot \vec{\rho}_1)}{R^2} \right] + \dot{\rho} \\ \frac{c_1 m_2 + c_2 m_1}{m_2} &= - \left[ \frac{Q_1}{m_1} \left\{ \dot{\vec{r}}_1 \times \vec{\nabla} \times \nabla \frac{\vec{M} \cdot \vec{r}_1}{r_1^2} - \frac{Q_2}{m_2} \left\{ \dot{\vec{r}}_2 \times \vec{\nabla} \left( \frac{\vec{m} \vec{r}_2}{r_2^2} \right) \right\} \right\} \right] \end{aligned} \quad (20)$$

$$\text{But, } \vec{r}_1 - \vec{r}_2 = \vec{\rho}_1 - \vec{\rho}_2 = \left( \frac{m_1 + m_2}{m_2} \right) \vec{\rho} \quad (21)$$

dividing throughout by  $\frac{m_1 + m_2}{m_2}$

$$\begin{aligned}
 & \ddot{\vec{\rho}} + \frac{\mu\vec{\rho}_1}{R^3} - \frac{3\mu\vec{R}(\vec{R}\cdot\vec{\rho}_1)}{R^5} + \frac{3\mu\kappa_2\vec{\rho}_1}{R^5} - \\
 & \frac{15\mu\kappa_2\vec{R}}{R^7}(\vec{R}\cdot\rho_1) + \lambda_\alpha \left[ 1 - \frac{\nu}{|\vec{\rho}_1|} \right] \vec{\rho}_1 \\
 & + \rho_a \dot{R} \dot{R} (c_1 - c_2) \frac{m_2}{m_1 + m_2} + \rho_a \dot{R} \left[ \dot{R} \left( \frac{\dot{R}\cdot\dot{\rho}_1}{R^2} + \vec{\rho}_1 \right) \frac{c_1 m_2 + c_2 m_1}{m_1 + m_2} \right] \\
 & = \frac{-m_2}{m_1 + m_2} \left[ \frac{Q}{m_1} \dot{\vec{r}}_1 \times \vec{\tau} \left\{ \frac{\vec{M}\cdot\vec{r}_1}{r_1^3} \right\} - \frac{Q_2}{m_2} \dot{\vec{r}}_2 \times \vec{\tau} \left\{ \frac{\vec{M}\cdot\vec{r}_2}{r_2^3} \right\} \right]
 \end{aligned} \tag{22}$$

Where  $\lambda_\alpha = \frac{m_1 + m_2}{m_1 m_2} \frac{\lambda}{l_0}$  (23)

$$\gamma = \frac{m_2 l_0}{m_1 + m_2}$$

Since  $\frac{1}{r_i^3} = \frac{1}{(r_i^2)^{3/2}} = \frac{1}{(r_i^2)^3 L} = \frac{1}{[(\vec{R} + \vec{\rho}_i)^2]^{3/2}}; i = 1, 2$

$$\begin{aligned}
 & = \frac{1}{R^3} - \frac{3\vec{R}\cdot\vec{\rho}_i}{R^5} \\
 & \frac{\vec{r}_i}{r_i^3} = (\vec{R} + \vec{\rho}_i) \left[ \frac{1}{R^3} - \frac{3\vec{R}\cdot\vec{\rho}_i}{R^5} \right]; i = 1, 2 \\
 & = \frac{\vec{R} + \vec{\rho}_i}{R^3} - \frac{3\vec{R}\cdot\vec{\rho}_i}{R^5} (\vec{R} + \vec{\rho}_i); i = 1, 2
 \end{aligned} \tag{24}$$

Hence, we have

$$\frac{Q_1}{m_1} \left\{ \dot{\vec{r}}_1 \times \vec{\nabla} \left( \frac{\vec{M}\cdot\vec{r}_1}{r_1^3} \right) \right\} \frac{Q_2}{m_2} \left\{ \dot{\vec{r}}_2 \times \vec{\nabla} \left( \frac{\vec{m}\cdot\vec{r}_2}{r_2^3} \right) \right\} = \vec{R} \times \vec{\nabla} \left( \frac{\vec{M}\cdot\vec{R}}{R^3} \right) \left( \frac{Q_1}{m_1} - \frac{Q_2}{m_2} \right) \tag{25}$$

Using (25) in (22) we obtain the linearized vector equation of motion for the particle of mass  $m_1$  comparative to the centre of mass of the structure in the procedure.

$$\begin{aligned} & \ddot{\vec{\rho}}_1 + \frac{\mu \vec{\rho}}{R^3} - \frac{3\mu \vec{R}(\vec{R} \cdot \vec{\rho}_1)}{R^5} + a_1 \vec{R} + a_2 \\ & \left[ \frac{\dot{\vec{R}}(\vec{R} \cdot \vec{\rho}_1)}{R^2} \dot{\vec{\rho}}_1 \right] + \frac{3\kappa_2 \mu \vec{\rho}}{R^5} - \frac{15\mu \kappa_2 \vec{R}(\vec{R} \cdot \vec{\rho}_1)}{R^7} + \lambda_\alpha \left[ 1 - \frac{r^3}{|\vec{\rho}_1|} \right] \vec{\rho}_1 \\ & \frac{-m_2}{m_1 + m_2} \left[ \vec{R} \times \vec{\nabla} \left( \frac{\vec{M} \cdot \vec{R}}{R^3} \right) \left( \frac{Q_1}{m_1} - \frac{Q_2}{m_2} \right) \right] \end{aligned} \quad (26)$$

The condition of constraint given by (1) reduces to

$$|\vec{\rho}_1|^2 \leq v^2 \quad (27)$$

If in (27) the system will be moving with moveable string if the inequality sign is true (Thakur, 1959). In this case, the motion is free from constraint and hence  $\lambda_\alpha = 0$ . If the equality signs in (27) holds then the motion is constrained motion and hence  $\lambda_\alpha \neq 0$ . (Etkin, 1964).

Let us stabilize the vector  $\vec{\rho}_1$  by familiarizing.

$$\vec{\rho}_1 = \frac{v \vec{\rho}_1^*}{l_0}$$

(28)

Then the vector equation (26) of the particle of mass  $m_1$  takes the form

$$\ddot{\vec{\rho}}_1^* + \frac{\mu}{R^3} \vec{\rho}_1^* - \frac{3\mu \vec{R}(\vec{R} \cdot \vec{\rho}_1^*)}{R^5} + a_1 \dot{\vec{R}} + a_2 \left[ \frac{\dot{\vec{R}}(\vec{R} \cdot \dot{\vec{\rho}}_1^*)}{R^2} + \dot{\vec{\rho}}_1^* \right]$$

$$\begin{aligned}
 & + 3\mu\kappa_2\vec{\rho}_1^* - \frac{15\mu\kappa_2\vec{R}}{R^7}(\vec{R}\cdot\vec{\rho}_1^*) + \\
 \lambda_\alpha \left[ 1 - \frac{l_0}{|\vec{\rho}_1^*|} \right] \vec{\rho}_1^* & = -\vec{R} \times \vec{\nabla} \left( \frac{\vec{M}\cdot\vec{R}}{R^3} \right) \left( \frac{Q_1}{m_1} - \frac{Q_2}{m_2} \right)
 \end{aligned} \tag{29}$$

Where  $a_1 = \frac{a_1'(m_1 + m_2)}{m_2} = \rho\alpha R(c_1 - c_2)$

$$a_2 = \frac{a_2^1(m_1 + m_2)}{m_2} = \rho\alpha R \frac{(c_1 m_2 + c_2 m_1)}{m_2} \tag{30}$$

The system's mass center and the stabilized vector equation of the relative motion of the particle of mass  $m_1$  (Hagihara, 1957).

Now the condition of constraint given by (28) takes the form

$$|\vec{\rho}_1^*|^2 \leq l_0^2 \tag{31}$$

Again, let us write

$\vec{\kappa}E$  = unit vector along the axes of the magnetic dipole of the earth

$$= \frac{\vec{M}}{|\vec{M}|}$$

$u_E$  = The volume of the magnetic moment of the earth dipole M

$\vec{\rho}_r$  = unit vector along the radius vector  $\vec{R}$

$$= \frac{\vec{R}}{|\vec{R}|} \text{ where } \vec{R} \text{ is the radius vector of the centre of mass of the system with}$$

respect to the appealing center of force.

Hence, equation of motion given by (29) takes the form

$$\vec{\rho}_1^* + \frac{\mu}{R^3}\vec{\rho}_1^* - \frac{3\mu\vec{R}}{R^5}(\vec{R}\cdot\vec{\rho}_1^*) + a_1\vec{R} + a_2 \left[ \frac{\dot{\vec{R}}(\vec{R}\cdot\vec{\rho}_1^*)}{R^2} + \dot{\vec{\rho}}^* \right] + \frac{3\mu\kappa_2}{R^5}\vec{\rho}_1^* -$$

$$\begin{aligned} & \frac{15\mu\kappa_2}{R^7} \vec{R}(\vec{R} \cdot \vec{\rho}_1^*) + \lambda_\alpha \left[ 1 - \frac{l_0}{|\vec{\rho}_1^*|} \right] \vec{\rho}_1^* \\ &= - \left( \frac{Q_1}{m_1} - \frac{Q_2}{m_2} \right) \left[ \frac{\mu E^R}{R^3} \times \vec{\kappa} E - 3(\vec{\kappa} E \cdot \vec{\rho}_1) \vec{R} \times \vec{\rho}_r \right] \end{aligned} \quad (32)$$

Our consideration of equation (32) leads us to the conclusion that there are two terms that make up atmospheric drag: one with coefficient  $a_1$  and the other with coefficient  $a_2$  (Leipholz, 1980). The dissipative force, which is a component of atmospheric drag resulting from air friction, is shown by the phrase with coefficient  $a_2$  with  $\vec{\rho}_1^*$  as a factor. We may disregard these terms as the coefficient  $a_2$  a parameter of the aerodynamic force, is a small quantity that is multiplied by a small quantity  $\vec{\rho}_1^*$  since we are just examining first-order turbulence. Furthermore, if we continue using this dissipative phrase, it will be hard to solve this topic analytically

Thus, the equation of motion (32) with only non-dissipative part of the aerodynamic force (Austin, 1965) takes the form

$$\begin{aligned} & \ddot{\vec{\rho}}_1^* + \frac{\mu}{R^3} \vec{\rho}_1^* - \frac{3\mu}{R^5} \vec{R}(\vec{R} \cdot \vec{\rho}_1) + a_1 \dot{\vec{R}} + \frac{3\mu\kappa_2}{R^5} \vec{\rho}_1^* - \frac{15\mu\kappa_2}{R^7} \vec{R}(\vec{R} \cdot \vec{\rho}_1^*) + \lambda_\alpha \left[ 1 - \frac{l_0}{|\vec{\rho}_1^*|} \right] \vec{\rho}_1^* \\ &= - \left( \frac{Q_1}{m_1} - \frac{Q_2}{m_2} \right) \left[ \frac{\mu_E \vec{R}}{R^3} \times \vec{\kappa}_E - 3(\kappa_E \cdot \vec{\rho}_r) \vec{R} \times \vec{\rho}_r \right] \end{aligned} \quad (33)$$

### Conclusion

This equation (33) is the basic equation of motion of the particle of mass  $m_1$  of the system. The motion of the other particle of mass  $m_2$  can be easily obtained with the help of

$$m_1 \vec{\rho}_1 + m_2 \vec{\rho}_2 = 0$$

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