

Design, fabrication and testing of hydro turbine with composite path runner for ultra-low head application

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ABSTRACT

This paper is focused on design a turbine with composite path runner for ultra low head application and finally analyze its performance under different test conditions. Literature review was the starting point of research and detailed design parameters for the turbine dimensions and materials were selected taking feasibility of fabrication and testing in hand. The testing was proposed on real site of Bagmati river at Kupandole, Lalitpur, Nepal where the turbine was subjected to fuse ree-flowing water from the head of 1.3m and flowrate of 78 LPS that taken as site parameter. The 3D model for the turbine was developed in CATIA. For turbine height of 0.77m and runner minor diameter of 0.152m, simulations were carried out to find the most feasible number of blades, blade width, blade spacing, number of guide vanes and guide vane spacing using ANSYS simulation. Among the simulation the best arrangement was blade radial width of 62 mm, blade spacing of 54mm, guide vane spacing of 36.5 mm, total number of blades 25 and total number of guide vanes 7 keeping output power in mind. The experimental results were then compared with the data obtained from calculations and simulations. Turbine at part load of $Q_0/Q_{max} = 0.67$ was tested and the resulting maximum efficiency was 21.1% at 87 RPM with available flow rate of 52 LPS.

Keywords: ANSYS, CATIA, Composite path, Ultra low head, part load, LPS

INTRODUCTION

Rural electrification is often conjoined with optimal use of locally available resources like ultra low head resources in mountainous country Nepal, transmission of remotely generated power to unevenly distributed villages seems costlier [1]. Conceding with this fact, low and ultra low head are being used to satiate current power demand. Ultra-low head is the situations where the hydraulic head is less than 3 m or the water flow is more than 0.5 m/s with zero head [2]. Locally established water mills and hydropower plants using Archimedean Screw Turbine and Gravitational vortex plant are the good example of them. They are basically suitable for plain region of the country [3]. Composite path runner turbine works prominently on impulse principle.

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Problem statement

It is self evident that rural electrification can be achieved effectively by using locally available resources to the country like Nepal where demographical distribution is largely uneven. Especially in Terai region of country, there seems no valuable technological study to tap the energy from water resources flowing near-by them. So, this research aims to develop a low scale hydro turbine that might be a mile stone for developmental step.

Research objective

- i. To design and simulate turbine with composite path runner for head of 1.3m and 78 LPS.
- ii. To fabricate complete turbine system as per design.
- iii. To test the performance of turbine at real site condition.

Literature review

Turbine uses symmetrically curved vanes that are mounted to pair of continuous power transmission belts each of which revolves on a pair of grooved pulleys. The blades move in substantially linear paths on both the upstream and downstream sides where water strikes, which extend between the circumference of top and bottom pulley. In first series of blade, impulsive force is created that makes the blade move downward while at second series of blade, reactive force is generated which makes the blade move upward, resulting the runner to rotate generating mechanical power. Power generation from the turbine is based on Euler's turbine equation [4].

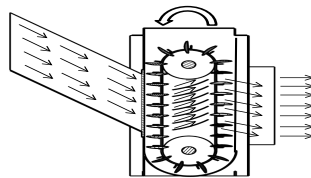


Fig: Schematic diagram demonstrating turbine working principle

Natel energy Inc of United states patented first turbine based upon composite path runner [5]. They used runner with symmetrically curved vanes mounted on a timing belt which would revolve on a pair of axles.

- Eberhard of Switzerland also developed turbine based upon the same principle that the blades that contribute to power output travel in the same direction as the fluid flow 50%.

Nance of US also developed similar two stage turbines. In his invention the blades in the second stage are situated to receive direct input of fluid as well as fluid directed from the front blades after glancing off of them but his design suffered with confluent flow condition with two streams of flow.

Schneider with the objective to provide an improved system, method, and apparatus for a linear hydraulic impulse machine developed a linear hydraulic machine which utilizes reaction foils, operating with the principle of lift [6].

Research Methodology

- Problem identification
- Literature review
- Field identification for design parameter
- Design and simulation of turbine
- Fabrication of system
- Testing of the system
- Result analysis
- Final conclusion and recommendation

Design Summary**Blade design**

- Blade was designed with the basic relation of inlet and blade angle from cross flow turbine which is, $\tan(\beta)=2 * \tan(\alpha)$ [8].
- Suitable angle of water velocity was chosen by performing ANSYS simulation.

6.2 Runner design

Head	1.3m
Flow rate (maximum possible to divert)	78 LPS
Velocity	3.25 m/s
Density of water	1000 kg/m ³

Water inlet angle selected

- Pitch circular diameter (PCD) calculated and inner and outer diameter of blade determined. $=$ and $D_i/D_o = 0.66$ [7]
- Blade radial width is selected through difference of inner to outer diameter.
- Blade spacing determined through simulation
- Distance between shaft centers determined

6.3 Formulae for shaft design

Marin equation for endurance limit of shaft	$= (K_a * K_b * K_c * K_d * K_e * K_f * S_e')$
Catalogue load rating (C_{10}) for bearing	$C_{10} = F_D \left[\frac{x_D}{x_D + (\theta - x_0)(1 - R_D)^{1/b}} \right]^{1/b}$
Head loss due to friction	$\Delta h_f = f \frac{LV^2}{2gD_e}$
Reynolds's no	$\frac{\rho D_e v_{avg}}{\mu}$
diametric ratio	$\frac{D_i}{D_t} = 0.66$
Impulsive Force on blade	$F1 = \rho * Q * (V_{w1} - V_{w2})$

[9,10, 11, 12]

Taking factor of safety (n) as 13.55, the diameter of shaft is found to be 25 mm. The diameter of safety is taken in such a way that is will be easy for manufacturing taking account of safety requirements.

6.4 Calculation result

Inlet dimension	200mm * 300 mm
Velocity of water at inlet	3.25 m/s
Force on first series of blade	226.2 N
Force on second series of blade	55.38 N
Ultimate tensile strength of blade material (1020 CD)	470 MPa
Actual flow rate	52 LPS

CFD analysis of model

$$d = \left[\frac{16n}{\pi} \left\{ \frac{1}{S_e} [4(K_f * M_a)^2 + 3(K_{fs} * \tau_a)^2]^{1/2} + \frac{1}{S_{yt}} [4(K_f * M_m)^2 + 3(K_{fs} * \tau_m)^2]^{1/2} \right\} \right]^{1/3}$$

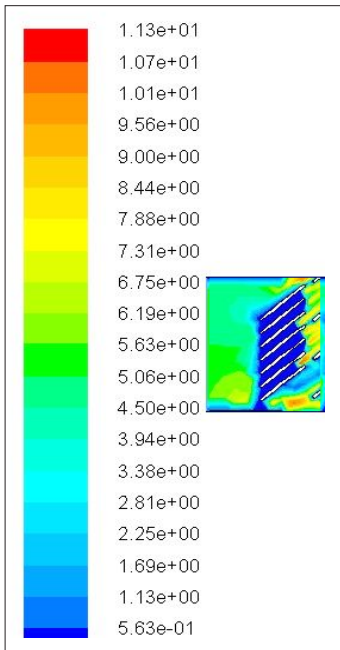


Fig: Velocity contour for

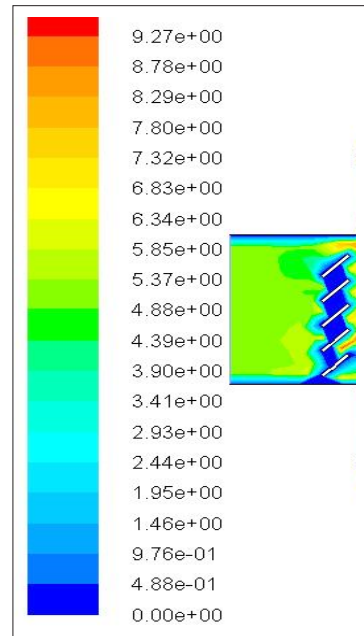


Fig: Velocity contour for 30mm blade spacing

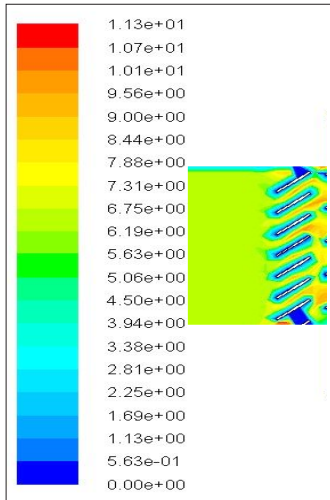
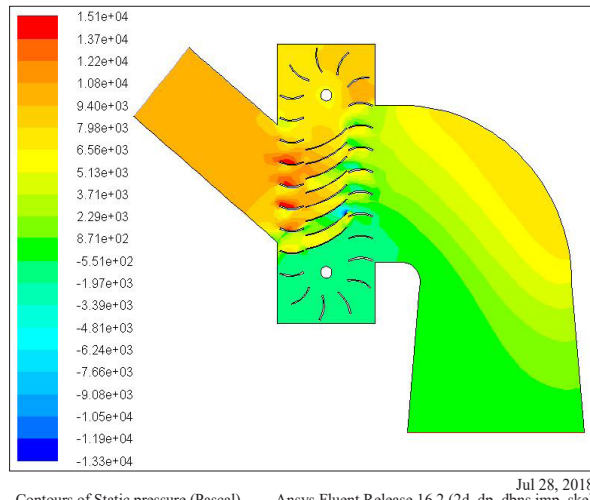


Fig: Velocity contour for 35 mm blade spacing



Contours of Static pressure (Pascal) Ansys Fluent Release 16.2 (2d, dp, dbns imp. ske)

Fig: Pressure contour in turbine (Pa)

CFD simulation showed that the system has more efficiency when draft tube is used. To validate that with experiment, the tests were aimed to conduct at Bagmati River near Kupandole Bridge.

Fabrication

Penstock, casing, runner and brake dynamometer were fabricated and assembled. Mild steel was used primarily to fabricate them. Different standard machine tools were used for fabrication of the complete system.

Testing and Data Analysis

9.1 Site description:

Testing of turbine was done at real site on Bagmati River at Kupandole, Lalitpur, Nepal. Suitable arrangement for the placement of turbine and other accessories on the safe side of river was made for ease of testing. The testing instruments and test sheet were made prepared for data measurement.

9.2 Measurement and data analysis

During preparation of test, flow arrangement was only possible up-to 52 LPS. So, it was tested in part load operating conditions. Brake dynamometer was used to measure the mechanical load and optical type tachometer was used to measure the rotational speed of the turbine. Various input and output parameters were measured and recorded on test sheet. Different test results obtained were plotted to develop various performance curve which are as following.

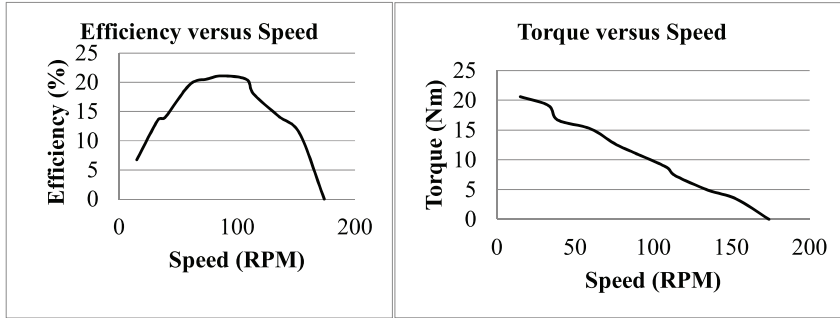


Fig: Variation of efficiency with speed

Fig: Variation of torque with speed

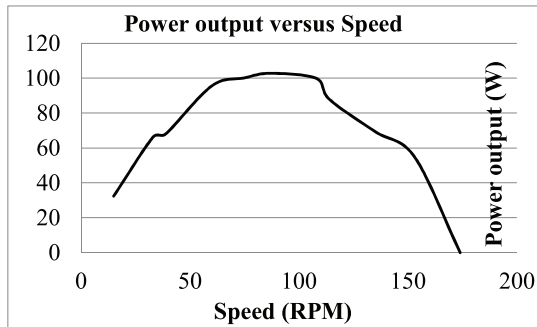


Fig: Variation of power output with speed

The maximum overall efficiency of the turbine was found to be 21.1% at 87RPM at the part load of $0.67Q_{max}$. If the required amount of flow could have been directed to turbine then the output of the turbine could have increased and so as the efficiency. From this result it was concluded that efficiency and power output graph found to be varied with speed, non-linearly. Linear relationship in between torque and speed denotes turbine can be operated on any speed without lose on torque. That makes it possible to operate turbine at speed satisfying maximum efficiency condition.



Fig: Testing of turbine

Conclusion

The system works better with draft tube rather than without draft tube.

The composite path runner really works with higher torque rather than the speed and generates mechanical power further that can be converted to electrical using speed increasing devices and generators.

Performance of turbine was tested for ultra-low head application with maximum efficiency of 21.1% at 87 RPM.

Recommendations

- a. Three-dimensional simulation of design can result more efficient blade profile.
- b. Manufacturing and selection of material properties can lead to better output.
- c. Testing on suitable test rig can result more accurate performance.

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