

“COMPUTATIONAL FLUID DYNAMICS ANALYSIS OF PENSTOCK BRANCHING IN HYDROPOWER PROJECT”

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Abstract

The penstock branching manifold is regarded as most critical part of the hydropower project. A computational research has been carried out to conclude the most efficient branching manifold with has more than or equal to three units of turbine. Starting from the base data from a project “Solukhola-Dudhkoshi Hydropower Project, 86 MW” for three units of turbines. More than 20 models were prepared to visualize flow pattern, to minimize the head loss and mas flow variation among 3 different units. The research has been finally concluded to go towards a single trifurcation instead of successive two bifurcation or individual branching form main branches.

Keywords: *Trifurcation, CFD, hydropower*

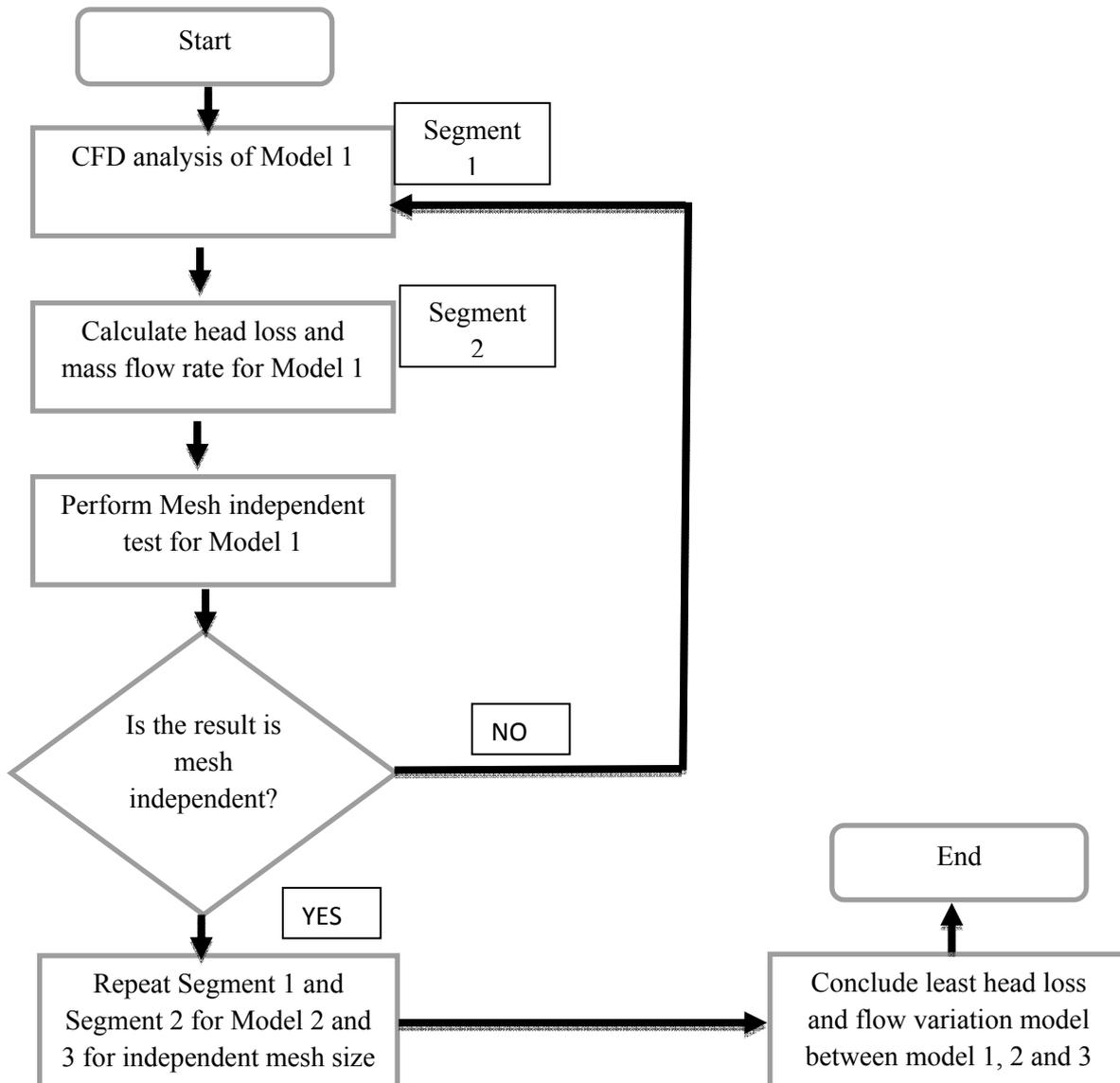
1. Background

In the hydropower project, a single generating unit is seldom chosen. The Turbines and generators needs periodic repair and maintenance. The shut down time required for the maintenance purpose is the time the generation will be lost. In case of single unit, the plant generation loss for the maintenance will be huge. Hence, most of the plant will have at least two generating units. For more than 3 units of turbine the design of branching manifold will lead to greater study requirement, which is basically taken in consideration in the research. The base data has been taken from Solukhola-Dudhkoshi Hydropower Project, 86 MW as,

Table 1: Salient Properties of Project

Project	Solukhola (Dudhkoshi) HEP, 86 MW
Type of branching	Similar to Option 1
Design Flow Rate	17.505 cubic meter per second
Net Head	600 m
Angle of First Branching	68 degree
Angle of Second Branching	68 degree
Inside Diameter of Inlet Pipe	2.1 m
Inside Diameter of outlet Pipe	1.2 m

2. Methodology



3. Comparative study of 3 models

The 3 types of branching manifold were taken in the study to performing CFD analysis with the below mentioned boundary condition, meshing and analysis setup.

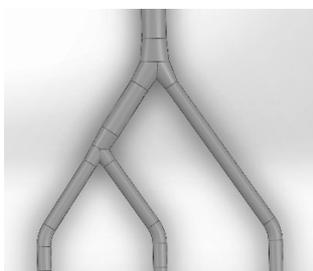


Fig 1: Branching Option 1

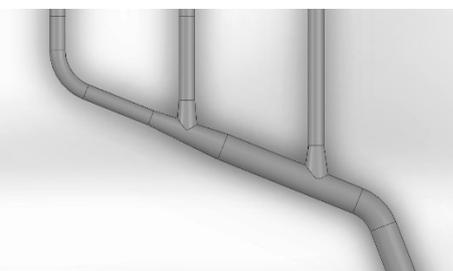


Figure 2: Branching Option 1

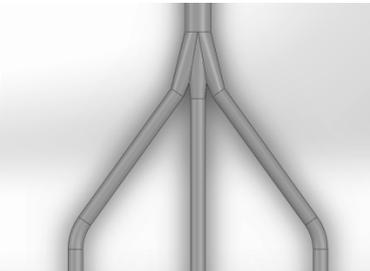
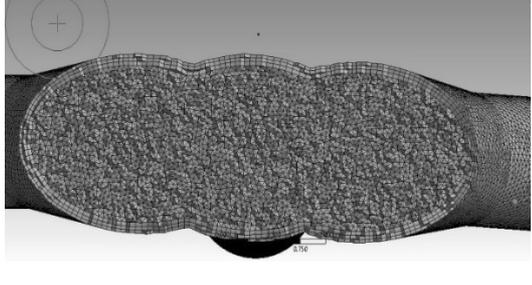


Figure 3: Branching Option 1

Table 2: Simulation and mesh setup for the analysis

Boundary Conditions		Simulation Setup	
Inlet		<i>Residual error :</i>	10 ⁻⁴
<i>Mass Flow rate (kg/s)</i>	17505	<i>Maximum iteration :</i>	200
Outlet		<i>Analysis type :</i>	Steady state
<i>Pressure Head (m)</i>	600	<i>Mass momentum :</i>	No slip wall
<i>Pressure (Pa)</i>	5868930.6	<i>Wall roughness :</i>	Smooth
Wall	No slip wall	<i>Turbulence model :</i>	Shear Stress Transport (SST)
Mesh Generation			
<i>Meshing type</i>	Tetrahedron		
<i>Body sizing</i>	50 mm		
<i>Smoothing</i>	High		
<i>Inflation</i>	Outer layer including boundary layer		

Mesh Independent test:

The mesh independent test for the model 3 shows that all analysis can be performed with the mesh size of 50 mm.

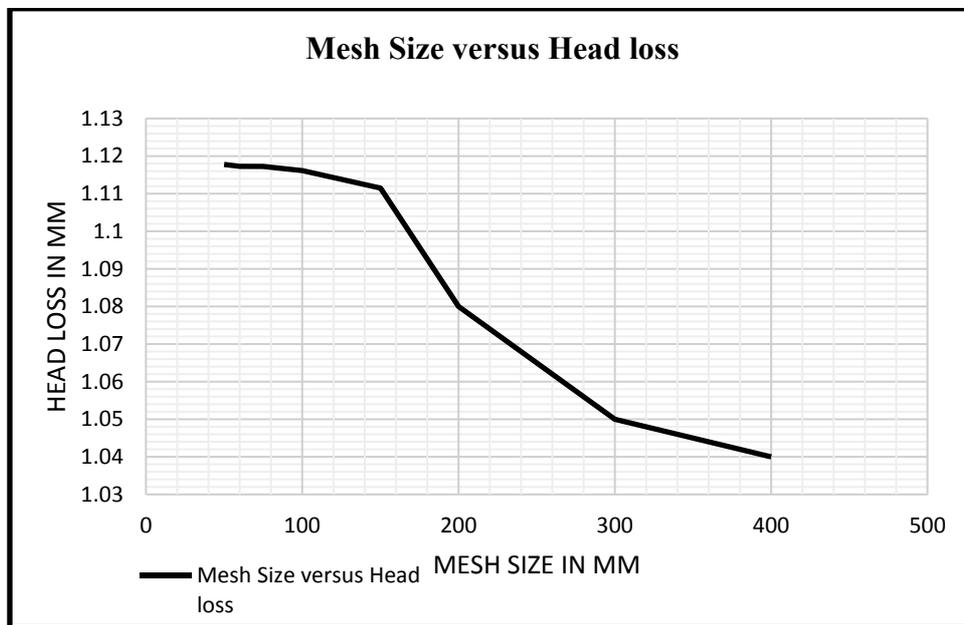


Fig 4: Mesh Independent test

4. CFD Analysis of Option 1

After performing simulation setup for the Option 1, it was put to target to achieve mentioned residual error target. The results are interpreted as below.

Pressure Distribution in Option 1:

The two images below shows the total pressure distribution within manifold. We can clearly see there is huge pressure drop in the confluence and below confluence of middle branch.

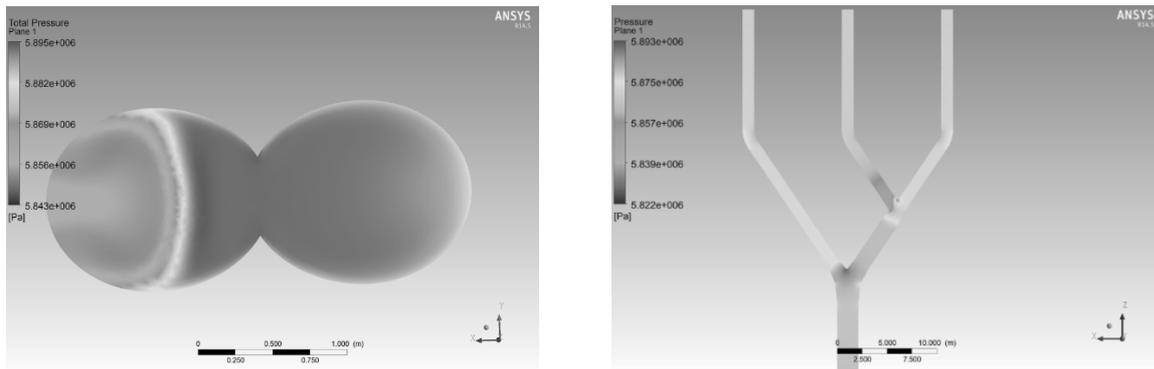


Fig 5 & 6: Pressure distribution in option 1

Velocity distribution in option 1:

The two figures below shows the velocity distribution in the branching manifold. The velocity lesser in the middle branch have led the mass flow difference (lesser in branch 1)

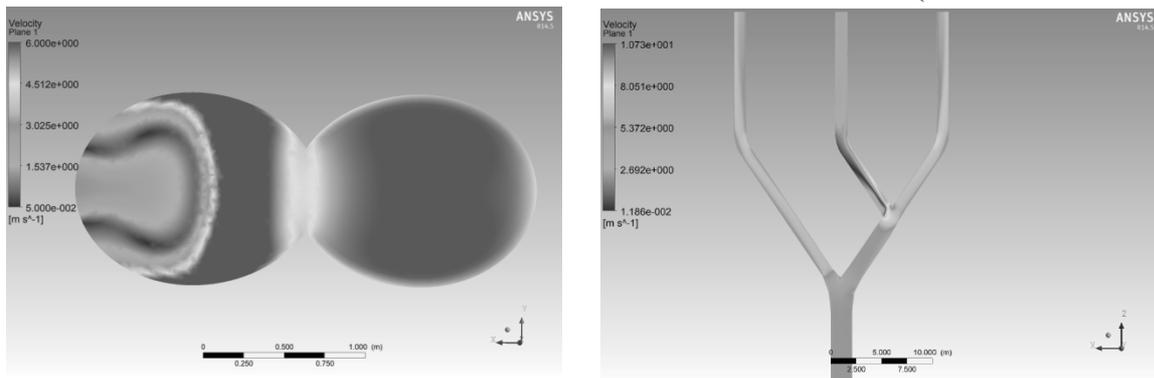


Fig 7 & 8: Velocity distribution in option 1

5. CFD Analysis of First Option 2

After performing simulation setup for the Option 2, it was put to target to achieve mentioned residual error target. The results are interpreted as below.

Pressure Distribution in option 2:

The total pressure in the branch 1 and branch 2 seems to be slightly lower as per the two figures below.

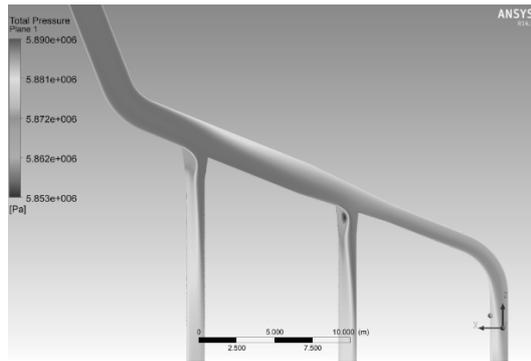


Fig 9: Pressure distribution in option

Velocity distribution in option 2:

The velocity distribution in the option 2 is described by the figure below.

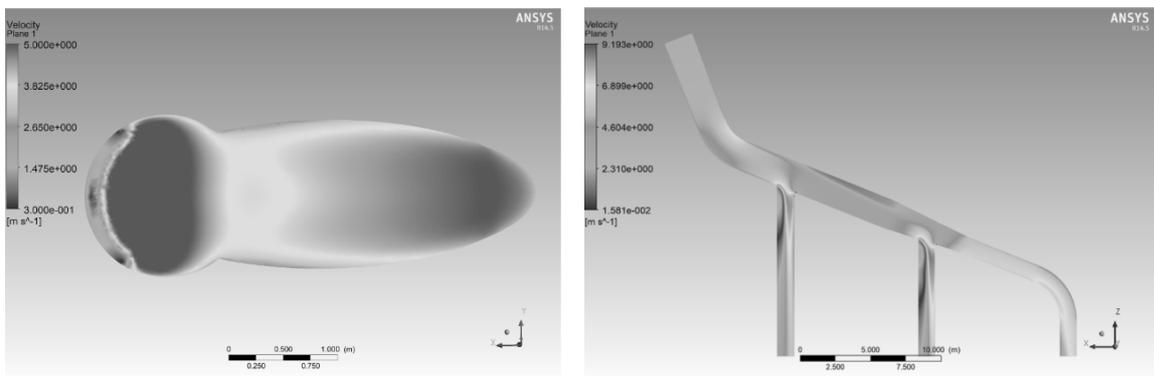


Fig 10 & 11: Velocity distribution in option 2

6. CFD Analysis of First Option 3

After performing simulation setup for the Option 2, it was put to target to achieve mentioned residual error target. The results are interpreted as below.

Pressure Distribution in option 3:

The total pressure distribution seems to be more identical throughout the branches as per figures below.

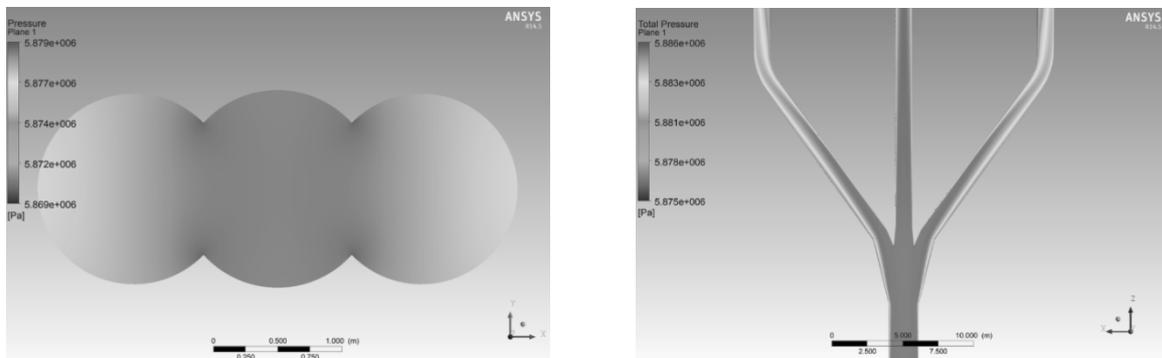


Fig 12 & 13: Pressure distribution in option 3

Velocity distribution in option 3

The velocity is lower in trifurcation junction, and the other distribution can be well described as per the figure below.

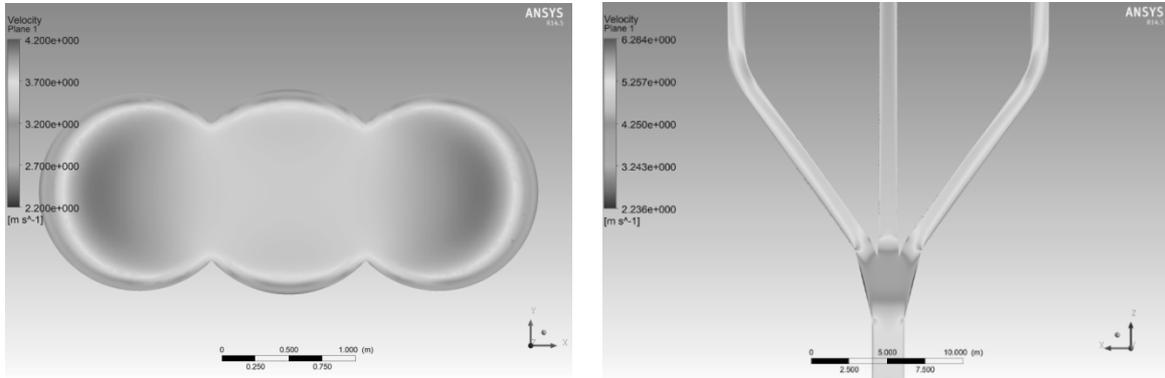


Fig 14 & 15: Velocity distribution in option 3

7. Comparative Analysis for 3 Types of Branching

Two parameters head loss and mass flow variation within the units have been calculated to analyze the performance of 3 types of branching. Similar analysis setup, meshing setup, boundary condition were applied to conclude the following result.

Table 3: The comparison of CFD simulation between all branches type

S.N	Types of Branching	Total Pressure comparison	Velocity Comparison	Velocity Streamline comparison
1	Type 1	Total Pressure drop in the confluence and below confluence of middle branch	The velocity lesser in the middle branch have led the mass flow difference (lesser in branch 1).	Low velocity zone in the middle branch
2	Type 2	The total pressure in the branch 1 and branch 2 seems to be slightly lower	The velocity in the branch 1 and branch 2 seems to be slightly lower, after branching junction	Similar result, as velocity comparison
3	Type 3	The total pressure distribution seems to be more identical throughout the branches	The velocity is lower in trifurcation junction, and the other distribution are almost identical	Similar result, as velocity comparison

8. Analysis Result and Selection of the Branching:

CFD analysis were conducted for all 3 models with efficient profiles and the results are as per the table below. Which concludes the option 3 to be most efficient is chosen for detailed analysis.

Table 4: The comparison of 3 options in terms of head loss and mass flow variation.

S.N.	Types	Head loss	Mass flow	Variation occurred in
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			variation	
1	Option 1	0.987625 m	2982.65 Kg/s	Middle branch
2	Option 2	0.624134 m	919.4 Kg/s	Middle branch
3	Option 3	0.309971 m	278.69 Kg/s	Both Side branches

9. Conclusions

3 basic designs were prepared as per the normal branching practice for 3 units of turbine. With proper CFD simulation methodology, pressure, velocity, head loss and mass flow variation were studied to conclude most efficient branching among all three. The first concludes 0.987625 m head loss and 2982.65 kg/s mass flow variation in first type, 0.6241 m and 919.4 kg/s mass flow variation in second type and 0.309971 m and 278.69 kg/s in third type of branching respectively. The study recommends to perform further intense study in third type of branching.

10. Recommendations

All the results are mostly site specific, not exact results but analysis methods are recommended to be referenced in other projects before selection and design of penstock branching. It is recommended to design the branching section very carefully after generalizing or detailed analyzing basic parameters. After structural analysis the internal stiffener may cause the flow irregularity within branching, so the further detailed analysis must consider the case too.

11. References

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